## **letter**

## **Thermally activated deformation of polymers. Comments on a paper by Zhu and Zhu**

*Dear Sir* 

We have some reservations about the formulations and ideas presented in a paper by Zhu and Zhu<sup>1</sup>. These are discussed below.

(1) If  $V_a$  is the volume involved in an activation event (presumably the difference between the volume of the activated state and that of the normal state),  $V_a\tau$  ( $\tau$  is the applied shear stress) is not the work done by  $\tau$  during the process of activation and hence the free energy of activation  $\Delta G$  will not be reduced by that amount. This is due to the fact that a shear stress will not do any work unless there is a corresponding shear strain involved. Let this strain be  $\gamma_a$  (a tensorial component corresponding to  $\tau$ ) and let it be uniform within  $V_a$ . Then  $\Delta G$  is reduced by  $V_a \gamma_a \tau$  during the activation process. The product  $V_a\gamma_a$  is the activation shear strain volume  $\Omega_a$ . If  $\gamma_a$  is not uniform, a spatial integration is needed and if  $\Omega_n$  varies with  $\tau$  an integration with respect to  $\tau$  is needed as discussed before<sup>2,3</sup>. Now experimentally only  $\Omega$ <sub>2</sub> can be evaluated from a change of stress with strain rate.  $V_a$  can be estimated only by assuming a  $\gamma_a$  or vice versa.

(2) Zhu and  $Zhu^1$  assumed that the shear strain produced by each activation event is:

$$
\gamma_{\rm p} = \beta_2 \frac{V_{\rm a}}{V_{\rm m}} \times \frac{\lambda}{\lambda_1} \tag{1}
$$

where  $\lambda/\lambda_1$  is the shear strain produced in  $V_a$  after the completion of the activation event,  $V_m$  is the volume of the molecular chain and  $\beta_2$  is a factor used to convert the local strain to the system strain, namely, the number of activation events within the molecular chain per unit time interval. Since  $V_a$  should be  $\Omega_a$  or  $V_a\gamma_a$ , this assumption is really:

$$
\gamma_{\rm p} = \beta_2 \frac{V_{\rm a} \gamma_{\rm a}}{V_{\rm m}} \times \frac{\lambda}{\lambda_1} \tag{2}
$$

which, when combined with their equation (2), gives the following strain rate:

$$
\dot{\gamma}_{\rm p} = \gamma_{\rm p} v_{\rm r} = \beta_1 \beta_2 \left(\frac{kT}{h}\right) \left(\frac{V_{\rm a} \gamma_{\rm a}}{V_{\rm m}}\right) \left(\frac{\lambda}{\lambda_1}\right)
$$

$$
\exp\left(-\frac{\Delta G}{kT}\right) \sinh\left(\frac{\Omega_{\rm a} \tau}{kT}\right) \tag{3}
$$

The minus sign in front of  $\Delta G$  is missing in their equation (4); their  $V_a$  has been replaced by  $\Omega$ <sub>a</sub> which was assumed constant in order to obtain the hyperbolic sine function. Then they assumed a value of 2 for  $\beta_1\beta_2\lambda/\lambda_1$ . The justification was that the rate equation will not be affected much whether the value 2 is 0.2 or 20. Unfortunately the activation entropy calculation depends directly on that assumption. For example, a factor of 10 increase in the pre-exponential reduces the activation entropy by  $R \ln(10)$  per mole where  $R$  is the gas constant.

(3) In deriving their equations (12) and (13) they assumed  $\Delta H$ ,  $V_a$  and  $\Delta S$  to be constants (not varying with either temperature or strain rate). However, their Figures 4, 5 and 6 show clearly that these quantities vary with both temperature and strain rate. However, if expressed properly<sup>2</sup>, these quantities do not have to be assumed constant in order to evaluate them.

(4) While their equation (14) was derived by Ferry<sup>4</sup> from the WLF equation except for a sign in the denominator:

$$
\Delta H_{\rm m} = \frac{2.303RC_1C_2T^2}{(T - T_{\rm g} + C_2)^2} \tag{4}
$$

their equation (15) was their own creation. They used the idea that  $T<sub>g</sub>-C<sub>2</sub>$  is a thermodynamic transition temperature so that:

$$
\Delta S_{\rm m} = \Delta H_{\rm m}/(T_{\rm g} - C_2) \tag{5}
$$

at this temperature. In this case since  $\Delta H_{\text{m}}$ approaches infinity so does  $\Delta S_m$  at  $\hat{T} = T_g - C_2$ . Furthermore this idea does not give  $\Delta S_m$  at other temperatures. Their equation  $(1\overline{5})$  shows:

$$
\Delta S_{\rm m} = \frac{\Delta H_{\rm m}}{T^2} (T_{\rm g} - C_2) \tag{6}
$$

at other temperatures. This equation requires justification.

(5) The flow of a liquid is homogeneous on the molecular scale but the flow of a solid is inhomogeneous. Shear bands and crazes are clearly visible even by human eyes. To regard the plastic deformation of glassy polymers as a viscous flow of a supercooled melt will not help us understand their differences. In fact Zhu and Zhu do not really have any evidence for this similarity.

Donyau Chiang and James C. M. Li *Materials Science Program, Department of Mechanical Engineering, University of Rochester, Rochester, NY 14627, USA* 

## REFERENCES

- 1 Zhu, X. X. and Zhu, G. R. *Polymer* 1992, 33, 4968
- 2 Li, J. C. M., Pampillo, C. A. and Davis, L. A. in 'Deformation and Fracture of High Polymers' (Eds H. H. Kausch, J. A. Hassell and R. I. Jaffee), Plenum Press, New York, 1973, pp. 239-258
- 3 Li, *J. C. M. J. AppL Phys.* 1971, 42, 4543
- 4 Ferry, J. D. 'Viscoelastic Properties of Polymers', 3rd Edn, Wiley, New York, 1980, p. 289

0032-3861/94/21/4702-01 © 1994 Butterworth-Heinemann Ltd **4702** POLYMER Volume 35 Number 21 1994